## Quiz 4

Chemical Engineering Thermodynamics
February 11, 2016

P4.2. Twenty molecules are contained in a piston + cylinder at low pressure. The piston moves such that the volume is expanded by a factor of 4 with no work produced of any kind. Compute $\Delta \mathrm{S} / \mathrm{k}$ in two ways, a) using four separated initial volumes and calculating the number of states in the initial and final conditions, and b) by considering the ratio of the initial and final volumes. Why do the two answers differ and why is one larger?
4.9. Airplanes are launched from aircraft carriers by means of a steam catapult. The catapult is a well-insulated cylinder that contains steam, and is fitted with a frictionless piston. The piston is connected to the airplane by a cable. As the steam expands, the movement of the piston causes movement of the plane. A catapult design calls for 270 kg of steam at 15 MPa and $450^{\circ} \mathrm{C}$ to be expanded to 0.4 MPa . How much work can this catapult generate during a single stroke? Compare this to the energy required to accelerate a 30,000 kg aircraft from rest to 350 km per hour.
$\mathrm{R}=8.314 \mathrm{~J} / \mathrm{mole}-\mathrm{K} ; \mathrm{N}_{\mathrm{A}}=6.022 \times 10^{23} ; \mathrm{N}_{\mathrm{A}} \mathrm{k}_{\mathrm{B}}=\mathrm{R}$;
1 Joule $=1 \mathrm{~N}-\mathrm{m}=1 \mathrm{MPa}-\mathrm{cm}^{3}=1 \mathrm{~kg} \mathrm{~m} / \mathrm{s}^{2}=0.23901 \mathrm{cal}$

## E.9. Properties of Water ${ }^{1}$

## I. Saturation Temperature

| $\begin{gathered} T \\ \left({ }^{\circ} \mathrm{C}\right) \end{gathered}$ | $\begin{gathered} P \\ \left(M P_{2}\right) \end{gathered}$ | \% $m^{\prime} / \mathrm{lg}$ | $\begin{gathered} 1^{r} \\ m^{3} / \mathrm{kg} \end{gathered}$ | 4 Wkg | $\begin{aligned} & \Delta U^{\text {eq }} \\ & \mathrm{NHg} \end{aligned}$ | $V^{F}$ $\mathrm{Wh}$ | $H$ <br> Nk | $\begin{aligned} & \mathrm{N} /{ }^{-\mu} \\ & \mathrm{N} \mathrm{l}_{8} \end{aligned}$ | $\\|^{\prime}$ $\mathrm{NH}_{\mathrm{g}}$ | 5 <br> $\mathrm{Nl}_{4}-\mathrm{K}$ | $\begin{gathered} \Delta 5^{\circ} \\ \text { Wlof } \end{gathered}$ | 5 <br> $\mathrm{Nl}+-\mathrm{K}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.01 | 0.00612 | 0.001500 | 2169912 | 0.00 | 237492 | 237492 | 0.00 | 250092 | 250092 | 0.000 | 9.1565 | 91555 |
| 5 | 0.00873 | 0.061000 | 147.013 | 2100 | 236076 | 2381.78 | 21.0 | 249904 | 251006 | 0.005 | 8948 | $9 \times 1045$ |
| to | (e901238 | 0.00600 | N63032 | 4208 | 234663 | 23 er 65 | 420 | 247719 | 251921 | 0.1511 | 87457 | 85088 |
| 15 | 0.00176 | 0.001001 | 77875 | 628 | 233251 | 2395.8 | 6298 | 246535 | 2588.33 | 0225 | 8559 | 87803 |
| 20 | 000339 | 0.00100 | 57.1569 | 8391 | 231841 | 24023 | 8391 | 24955 | 23374 | eves | 83008 | stete |
| 25 | 0.003170 | 0.00103 | 433973 | 10483 | 230430 | 240913 | 10483 | 24168 | 254551 | 03672 | 8.1894 | 85566 |
| 30 | 0.00247 | 0001004 | 32878 | 126.73 | 229018 | 241591 | 12673 | 24098 | 255555 | 0.438 | 80152 | 81530 |
| 35 | enebs\% | 0961006 | 23063 | 14663 | 22\%04 | 20269 | 14663 | 24179 | 29645 | OSMOI | 18106 | 83517 |
| 45 | 0,00739 | 0.01008 | 195151 | 16753 | 228185 | 242939 | 16753 | 200598 | 257351 | 05724 | 76831 | 82555 |
| 45 | 0009595 | 0.001010 | 152521 | 188.43 | 224765 | 246608 | 188.4 | 23960 | 25824 | 063\% | 75397 | 81613 |
| 5 | 0.012400 | 0.001012 | 12039 | 29033 | 233205 | 24273 | 20934 | 238198 | 2991.29 | 0.7038 | 13710 | 8074 |
| 55 | 0.015500 | 0001015 | 9.643 | 23024 | 221910 | 248934 | 20036 | 236083 | 250009 | 07680 | 12218 | 79508 |
| 60 | 601900 | 006tel | 1667 | 251.16 | 220474 | 246590 | 2518 | 235765 | NWE 83 | ${ }_{0} 8313$ | 1008 | 19031 |
| 65 | encoom | 0.001020 | 6.938 | 27209 | 219032 | 2662.41 | 27212 | 23638 | 261750 | 0s937 | 69399 | 789\% |
| 70 | 0031200 | 000102 | 50395 | 29318 | 217583 | 2468 \% | 20307 | 233303 | 26810 | -0651 | 6709 | 7754 |
| 75 | 0.03860 | 0.001036 | 41299 | 31399 | 2161.25 | 247524 | 31463 | 233057 | 33460 | 1.0158 | 66654 | 185812 |
| 80 | 0.arty | acoles | 3.025 | 34\% | 214680 | 248158 | 33801 | 230501 | 20450 | 107\% | 65345 | 76111 |
| 85 | 0.65790 | 0001032 | 2 E 58 | 35595 | 213186 | 245781 | 35601 | 220532 | 265139 | 1.145 | 64088 | 7544 |
| 90 | 0000200 | 0.00103s | 23991 | 37697 | 211700 | 249397 | 37104 | 208. 49 | 20959 | 1.1589 | 6285 | 1.888 |
| 96 | 0atise | 0.001045 | 1586 | $3 \% 6$ | 210204 | 250004 | 39809 | 22mes | 26761 | 1209 | 61647 | 7459 |
| 100 | 0.101400 | 0.001043 | 16718 | 419.0 | 2086\% | 25060 | 41917 | 2256.59 | 267557 | 13072 | 60469 | 13541 |
| 106 | 0.12090 | 0.001047 | 1.4184 | 44015 | 2071.78 | 281190 | 40127 | 22012 | 2083.39 | 1363 | 59319 | 72882 |
| 110 | 0.14400 | 600106? | 12093 | 45128 | 208641 | 281769 | 461.2 | 22064 | 269106 | 14188 | 58193 | 72398 |
| 115 | 0.169200 | 0.001656 | 10358 | 250.4] | 209592 | 252333 | 48.59 | 221509 | 209558 | 1473 | 5.001 | 7188 |
| 120 | 0.19590 | 0001060 | 08912 | 20360 | 200526 | 22588 | 50381 | 22012 | 27059 | 15290 | 56012 | 7129 |
| 125 | 0232200 | 0001065 | 2700 | 52483 | 2009.4 | 25427 | 53507 | 218803 | 271310 | 15816 | 5.454 | 710770 |
| 130 | 0270300 | 0.001080 | 06059 | 54609 | 1993.4 | 283959 | 54638 | 2173.70 | 272008 | 16345 | 53918 | 71064 |
| 138 | 0313800 | 003075 | 0.817 | S69,41 | 197724 | 25465 | 567.74 | 219913 | 278687 | 15572 | 5200 | 6977 |
| (4) | 0361500 | 0.001085 | 0.03s | 58871 | 190085 | 25996 | 58916 | 214428 | 2733.4 | 1.7392 | 5.901 | 69293 |
| 145 | 0.41500 | 0.001038 | 2486 | 65019 | 194423 | 254.4 | 610.64 | 212916 | 273080 | 1.8007 | 50919 | 6 sk 3 |
| 150 | 0.47600 | 0.06109 | 0.398 | 63166 | 192739 | 295908 | 63218 | 21138 | 27459 | 1848 | 4985 | 68371 |
| 155 | 0.54500 | 0.0010\% | 03458 | 65319 | 191032 | 26635 | 653.9 | 209808 | 275181 | 18 sed | 4900 | 6.985 |
| 160 | 0.4880 | 206150 | 0.208 | 6749 | 150299 | 2567.78 | 6754 | 208197 | 29578 | 1908 | 45065 | 6749 |
| 165 | 0.7000 | 0.001108 | 02724 | 65\% | 1575.99 | 257185 | 69734 | 246557 | 276281 | 1992 | 4714 | 6 Notb |
| 170 | 0.02200 | 0.001114 | 02486 | 718.20 | 155759 | 2575.73 | 71908 | 208882 | 276790 | 20417 | 4623 | 66650 |
| 175 | 0.925600 | 0.001121 | 02166 | 74008 | 183937 | 25793 | 7410 | 203169 | 27727 | 2006 | 45335 | 66541 |
| 150 | 1.00500 | 0.001127 | 01938 | 76152 | 18091 | 28858 | 763.05 | 201416 | 27721 | 2132 | 44485 | 65440 |
| 188 | 1.12300 | 0.mil3 | 21739 | 7391 | $15^{2} 13$ | 285804 | 78619 | 198\%2 | 2781.41 | 21875 | 43572 | 6547 |
| 190 | 123580 | 0.00114 | 01854 | 8060 | 178301 | 23sen | 807.13 | 197785 | 278838 | 2238 | 4.2704 | 65059 |
| 198 | 130850 | 0.6815 | 01499 | 888.18 | 1763.56 | 2991.74 | 88979 | 159903 | 27858 | 2285 | 4188 | 6.5578 |
| 20 | 158490 | 60.6159 | 01272 | 850.47 | 17837 | 2994.30 | 88.27 | 193974 | 27201 | 23305 | $409 \%$ | 6430 |
| 205 | 1.72430 | 0001164 | 0.1151 | 87287 | 172353 | 25\%40 | 8748 | 191955 | 27948 | $23 m$ | 40153 | 363930 |
| 210 | 190770 | 0.001173 | 0.104 | 805.39 | 10092 | 25831 | 897.6 | 189064 | 290121 | 2405 | 39818 | 863363 |
| 215 | 21058 | 0 0.0115 | 00047 | 91804 | 165190 | 25974 | 92153 | 187879 | 27033 | 25712 | 3858 | 8 6320 |
| 220 | 231960 | 0001190 | 0.561 | 98182 | 1660.43 | 300125 | 98358 | 185137 | 28005 | 25177 | 3763 | 3 6280) |
| 25 | 254970 | 0.001199 | 0.058 | 96.74 | 163850 | $3 \mathrm{SLD24}$ | 9688 | 183535 | 20215 | 2.564 | 3684 | 3 62483 |
| 230 | $2 \times 9710$ | 0.01509 | 0.015 | 96681 | 161609 | 3 SL 90 | 980.19 | 1812.71 | 20129 | 26101 | 36027 | 7 62128 |
| 235 | 306250 | 0.001219 | 0665 | 1010.4 | 1998.16 | $3 \times 13.20$ | 101307 | 1789.40 | 2303.17 | 26561 | 35214 | 46.1775 |
| 240 | 33450 | 000129 | 00697 | 1033.4 | 158969 | 3081.13 | 103755 | 1765.41 | 2012\% | 27030 | 34013 | 361423 |
| 245 | 365120 | $00012 \pm)$ | 00647 | 1057.12 | 155565 | 26067 | 106155 | 174067 | 20022 | 27978 | 3354 | 4.1072 |
| 250 | 39760 | 000128 | 00801 | 1080.79 | 1521.00 | $3 \mathrm{SOL.79}$ | 108577 | 1715.16 | 280093 | 2793 | 3278 | 6 60121 |
| 255 | 43290 | 0001264 | 0.469 | 1104.77 | 148572 | 2560.49 | 111023 | 1688 | 2790017 | 2898 | 31977 | 760369 |
| 260 | 468230 | 0.001276 | 0.422 | 112897 | 1499.75 | $25 \% 77$ | 1134\% | 1661.84 | 27\%60 | 2889 | 3.1167 | 760016 |
| 265 | 506330 | 0.001289 | 00387 | 1153.1] | 14364 | 25\%45 | 1159.9 | 163353 | 2783.49 | 29307 | 3035 | 45961 |
| 270 | 550360 | 0.001303 | 00356 | 1178.10 | 141557 | 2993.67 | 118527 | 1604.42 | 278969 | 2976 | 2959 | 99934 |
| 275 | 594640 | 0001318 | 00388 | 120307 | 138926 | 250.33 | 121090 | 1574.27 | 2755.17 | 31024 | 28720 | 58944 |
| 200 | 6.41660 | 000133 | 00302 | 12883 | 1358 \% | 2586.39 | 123688 | 1512.9 | 27758 | 30685 | 2784 | 158579 |
| 285 | 691470 | 000139 | 00.078 | 125392 | 13778 | 258181 | 12635 | 1510.48 | 2773.7 | 31147 | 2706 | 2 58009 |
| 29 | 7,4180 | 0001366 | 00056 | 127\% $\%$ | $12 \% 67$ | 25765 | 129003 | 147669 | 276670 | 31612 | 2622 | 25.784 |
| 295 | 799910 | 000135 | 0.035 | 1366.19 | 12 So 30 | 2570.49 | 131721 | 141.43 | 275870 | 32050 | 25371 | 15.751 |
| 300 | 8.58790 | 0001404 | 0.017 | 1322.95 | 123067 | 26636 | 135501 | 148.63 | 274964 | 3255 | 24507 | 75.7099 |
| 305 | 921940 | 0.00143 | 00199 | 1360.18 | 119567 | 255588 | 13730 | 1366.13 | 2739.4 | 33088 | 2369 | 56657 |
| 310 | 986310 | 000145 | 00088 | 13793 | 1199.14 | 2547.017 | 14022 | 135.73 | 27219 | 33510 | 2274 | 4 5634 |
| 315 | 1055600 | 0001472 | 00169 | 141628 | 118089 | 2537.17 | 19188 | 128322 | 271516 | 313078 | 21818 | 855816 |
| 330 | 112430 | 000159 | 00155 | 145531 | 1000.70 | 258601 | 14622 | 123837 | 270.59 | 3.4.4 | 21078 | 85597 |
| 38 | 12.05100 | 000158 | 00112 | 1475.11 | 103830 | 213.41 | 138358 | 119081 | 28433 | 3500 | 1000 | 85.508 |
| 330 | 1285810 | 0001561 | 0.013 | 150585 | 9883 | 249.15 | 158387 | 115016 | 2 6 66 B | 35618 | 1594 | 4 5402 |
| 335 | 13.01730 | 0001507 | 00118 | 1577\% | 98545 | $245 \%$ | 1559.45 | 10559 | 265535 | 36050 | 17856 | 6 53906 |
| 340 | 14.60070 | 0001688 | 0005 | 15706 | 8938 | 2454.4 | 159453 | 102732 | 2 S 159 | 36601 | 1.675 | 53336 |
| 35 | 155460 | 000168 | 00008 | 160530 | 877.09 | 24360 | 163148 | 96.12 | 29490 | 3.717 | 1556 | 6 52762 |
| 350 | 165990 | 0.00174 | 00088 | 169.13 | 71601 | 2418.14 | 167089 | 8275 | 26364 | 3774 | 1.488 | 652110 |
| 355 | 1757010 | 0.0158 | 0.0079 | 1681.5 | 766.4 | 238840 | 1713.72 | 81293 | 252665 | 3843 | 1.241 | 15130 |
| 360 | 1866600 | 0001505 | 0.009 | 17628 | 62550 | 2351.78 | 176166 | 71983 | 285189 | 39167 | 1.1399 | 50636 |
| 365 | 19.8210) | 0002017 | 0.060 | $177.7 \%$ | 52600 | 290379 | 1817.71 | 60518 | 20229 | 40014 | 09683 | 39497 |
| 370 | 21.04360 | 0002215 | 0.0050 | 184.07 | $3{ }^{3} 619$ | 2230.26 | 159069 | 4883 | 23458 | 41112 | 0.690 | 48012 |
| 37195 | 2206000 | 0.003106 | 0.0631 | 2015.73 | 0.00 | 2015.73 | 258426 | 0.00 | 2515.25 | 4.4070 | 0.000 | - 4.4070 |

## IL. Saturation Pressure

| $\begin{gathered} T \\ \left({ }^{\circ} \mathrm{C}\right) \end{gathered}$ | $\begin{gathered} P \\ (\mathrm{MPa}) \end{gathered}$ | $\mathrm{f}^{2}$ $\mathrm{~m}^{3} / \mathrm{kg}$ | $V^{V}$ $\mathrm{~m}^{3} / \mathrm{kg}$ | $U^{L}$ $\mathrm{~kJ} / \mathrm{kg}$ | $\begin{aligned} & \Delta U^{* N p} \\ & \mathrm{k} / \mathrm{kg} \end{aligned}$ | $U^{V}$ $\mathrm{~kJ} / \mathrm{kg}$ | $H^{2}$ <br> $\mathrm{k} / \mathrm{kg}$ | $\Delta H^{P V}$ <br> $\mathrm{k} / \mathrm{kg}$ | $\begin{gathered} H^{\prime V} \\ \mathrm{~W} / \mathrm{kg} \end{gathered}$ |  | $\begin{gathered} \Delta S^{* ण \varphi} \\ \mathrm{k} / \mathrm{kg} \cdot \mathrm{~K} \end{gathered}$ | $\begin{gathered} S^{V} \\ \mathrm{~W} / \mathrm{kg} \cdot \mathrm{~K} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6.97 | 0.001 | 0.001000 | 129.1780 | 29.30 | 2355.19 | 2384.49 | 29.30 | 248437 | 2513.67 | 0.1059 | 88690 | 8.9749 |
| 17.50 | 0.002 | 0.001001 | 66.9869 | 73.43 | 2325.47 | 2398.90 | 73.43 | 2459.45 | 253288 | 0.2606 | 8.4620 | 8.7226 |
| 24.08 | 0.003 | 0.001003 | 45.6532 | 100.98 | 2306.90 | 2407.88 | 100.98 | 2443.86 | 2544.84 | 03543 | 8.2221 | 8.5764 |
| 28.96 | 0.004 | 0.001004 | 34.7911 | 121.38 | 2293.12 | 2414.50 | 121.39 | 2432.28 | 2553.67 | 0.4224 | 80510 | 8.4734 |
| 32.87 | 0.005 | 0.001005 | 28.1853 | 137.74 | 2282.06 | 2419.80 | 137.75 | 2422.98 | 2560.73 | 0.4762 | 79176 | 83938 |
| 36.16 | 0.006 | 0.001006 | 23.7334 | 151.47 | 2272.76 | 2424.23 | 151.48 | 2415.15 | 2566.63 | 0.5208 | 78082 | 83290 |
| 39.00 | 0.007 | 0.001008 | 20.5245 | 163.34 | 2264.71 | 2428.05 | 163.35 | 2408.37 | 2571.72 | 0.5590 | 7.7155 | 8.2745 |
| 41.51 | 0.008 | 0.001008 | 18.0989 | 173.83 | 2257.58 | 2431.41 | 173.84 | 240237 | 2576.21 | 0.5925 | 7.6348 | 8.2273 |
| 43.76 | 0.009 | 0.001009 | 16.1992 | 183.24 | 2251.19 | 2434.43 | 183.25 | 239697 | 2580.22 | 0.6223 | 7.5635 | 8.1858 |
| 45.81 | 0.01 | 0.001010 | 14.6701 | 191.80 | 2245.36 | 2437.16 | 191.81 | 239205 | 2583.86 | 0.6492 | 7.49\% | 8.1488 |
| 60.06 | 0.02 | 0.001017 | 7.6480 | 251.40 | 2204.58 | 2455.98 | 251.42 | 235752 | 2608.94 | 0.8320 | 7.0752 | 7.9072 |
| 69.10 | 0.03 | 0.001022 | 5.2284 | 289.24 | 2178.46 | 2467.70 | 289.27 | 2335.28 | 2624.55 | 0.941 | 6.8234 | 7.7675 |
| 75.86 | 0.04 | 0.001026 | 3.9930 | 317.58 | 2158.75 | 2476.33 | 317.62 | 2318.43 | 2636.05 | 1.0261 | 6.6429 | 7.6690 |
| 81.32 | 0.05 | 0.001030 | 3.2400 | 340.49 | 2142.72 | 2483.21 | 340.54 | 2304.68 | 2645.22 | 1.0912 | 6.5018 | 75930 |
| 85.93 | 0.06 | 0.001033 | 2.7317 | 359.85 | 2129.10 | 2488.95 | 359.91 | 2292.95 | 2652.86 | 1.1455 | 6.3856 | 7.5311 |
| 89.93 | 0.07 | 0.001036 | 23648 | 376.68 | 2117.20 | 2493.88 | 376.75 | 2282.67 | 2659.42 | 1.1921 | 6.2869 | 7.4790 |
| 93.49 | 0.08 | 0.001039 | 2.0871 | 391.63 | 2106.58 | 2498.21 | 391.71 | 2273,47 | 2665.18 | 1.2330 | 6.2009 | 7.4339 |
| 9.69 | 0.09 | 0.001041 | 1.8694 | 405.10 | 209697 | 2502.07 | 405.20 | 2265.11 | 2670.31 | 1.2696 | 6.1247 | 73943 |
| 99.61 | 0.1 | 0.001043 | 1.6939 | 417.40 | 2088.15 | 2505.55 | 417.50 | 2257.45 | 2674.95 | 1.3028 | 6.0561 | 73589 |
| 120.21 | 02 | 0.001061 | 0.8857 | 504.49 | 2024.60 | 2529.09 | 504.70 | 2201.53 | 2706.23 | 1.5302 | 5.5967 | 7.1269 |
| 133.52 | 03 | 0.001073 | 0.6058 | 561.11 | 1982.04 | 2543.15 | 561.43 | 2163.45 | 2724.88 | 1.6717 | 5.3199 | 6.9916 |
| 143.61 | 0.4 | 0.001084 | 0.4624 | 604.22 | 1948.88 | 2553.10 | 604.66 | 213339 | 2738.05 | 1.7765 | 5.1190 | 6.8955 |
| 151.83 | 0.5 | 0.001093 | 0.3748 | 639.54 | 1921.17 | 2560.71 | 640.09 | 2108.02 | 2748.11 | 1.8604 | 4.9603 | 6.8207 |
| 158.83 | 0.6 | 0.001101 | 0.3156 | 669.72 | 1897.07 | 2566.79 | 670.38 | 2085.76 | 2756.14 | 1.9308 | 4.8285 | 6.7593 |
| 164.95 | 0.7 | 0.001108 | 0.2728 | 696.23 | 1875.58 | 2571.81 | 697.00 | 2065.75 | 2762.75 | 1.9918 | 4.7153 | 6.7071 |
| 170.41 | 0.8 | 0.001115 | 0.2403 | 719.97 | 1856.06 | 2576.03 | 720.86 | 2047.44 | 2768.30 | 2.0457 | 4.6159 | 6.6616 |
| 175.35 | 0.9 | 0.001121 | 0.2149 | 741.55 | 1838.09 | 2579.64 | 742.56 | 2030.47 | 2773.03 | 2.0941 | 4.5272 | 6.6213 |
| 179.88 | 1 | 0.001127 | 0.1944 | 761.39 | 1821.36 | 2582.75 | 762.52 | 201459 | 2777.11 | 2.1381 | 4.4469 | 6.5850 |
| 187.96 | 1.2 | 0.001139 | 0.1633 | 796.96 | 1790.87 | 2587.83 | 798.33 | 1985.41 | 2783.74 | 22159 | 4.3058 | 65217 |
| 195.04 | 1.4 | 0.001149 | 0.1408 | 828.36 | 1763.40 | 2591.76 | 829.97 | 1958.88 | 2788.85 | 22835 | 4.1840 | 6.4675 |
| 201.37 | 1.6 | 0.001159 | 0.1237 | 856.60 | 173823 | 2594.83 | 858.46 | 1934.36 | 2792.82 | 23435 | 4.0764 | 6.4199 |
| 207.11 | 1.8 | 0.001168 | 0.1104 | 882.37 | 1714.87 | 2597.24 | 884.47 | 1911.44 | 2795.91 | 23975 | 3.9800 | 63775 |
| 212.38 | 2 | 0.001177 | 0.09\% | 906.15 | 1692.97 | 2599.12 | 908.50 | 1889.79 | 2798.29 | 2.4468 | 3.8922 | 63390 |
| 223.95 | 2.5 | 0.001197 | 0.0799 | 958.91 | 1643.15 | 2602.06 | 961.91 | 1840.02 | 2801.93 | 25543 | 3.7015 | 6.2558 |
| 233.85 | 3 | 0.001217 | 0.0667 | 1004.69 | 1598.47 | 2603.16 | 1008.34 | 1794.81 | 2803.15 | 2.6456 | 3.5400 | 6.1856 |
| 242.56 | 3.5 | 0.001235 | 0.0571 | 1045.47 | 1557.47 | 2602.94 | 1049.80 | 175284 | 2802.64 | 27254 | 3.3989 | 6.1243 |
| 250.35 | 4 | 0.001253 | 0.0498 | 1082.48 | 1519.24 | 2601.72 | 1087.49 | 1713.33 | 2800.82 | 27968 | 3.2728 | 6.06\% |
| 257.44 | 4.5 | 0.001270 | 0.0411 | 1116.53 | 1483.15 | 2599.68 | 1122.25 | 1675.70 | 279795 | 28615 | 3.1582 | 6.0197 |
| 263.94 | 5 | 0.001286 | 0.0394 | 1148.21 | 1448.77 | 25\%6.98 | 1154.64 | 1639.57 | 2794.21 | 29210 | 3.0527 | 59737 |
| 275.59 | 6 | 0.001319 | 0.0324 | 1206.01 | 1383.89 | 2589.90 | 121392 | 1570.67 | 2784.59 | 3.0278 | 28623 | 5.8901 |
| 285.83 | 7 | 0.001352 | 0.0274 | 1258.20 | 1322.78 | 2580.98 | 1267.66 | 1504.97 | 2772.63 | 3.1224 | 26924 | 5.8148 |
| 295.01 | 8 | 0.001385 | 0.0235 | 1306.23 | 1264.25 | 2570.48 | 1317.31 | 1441.37 | 2758.68 | 32081 | 25369 | 5.7450 |
| 303.35 | 9 | 0.001418 | 0.0205 | 1351.1] | 1207.42 | 2558.53 | 1363.87 | 1379.07 | 2742.94 | 32870 | 23921 | 5.6791 |
| 311.00 | 10 | 0.001453 | 0.0180 | 1393.54 | 1151.65 | 2545.19 | 1408.06 | 1317.43 | 2725.49 | 33607 | 22553 | 5.6160 |
| 327.81 | 12.5 | 0.001546 | 0.0135 | 1492.26 | 1013.35 | 2505.61 | 1511.58 | 1162.73 | 2674.31 | 3.5290 | 1.9348 | 5.4638 |
| 342.16 | 15 | 0.001657 | 0.0103 | 1585.35 | 870.27 | 2455.62 | 1610.20 | 1000.50 | 2610.70 | 3.6846 | 1.6260 | 53106 |
| 354.67 | 17.5 | 0.001803 | 0.0079 | 1679.22 | 711.32 | 2390.54 | 1710.77 | 818.53 | 2529.30 | 3.8394 | 1.3037 | 5.1431 |
| 365.75 | 20 | 0.002040 | 0.0059 | 1786.41 | 508.63 | 2295.04 | 1827.21 | 585.14 | 241235 | 4.0156 | 0.9159 | 4.9315 |
| 373.95 | 22.06400 | 0.003106 | 0.0031 | 2015.73 | 0.00 | 2015.73 | 2084.26 | 0.00 | 208426 | 4.4070 | 0.0000 | 4.4070 |

## III. Superheated Steam

| $P=0.01$ | MPa | (45.8) |  |  | $P=00$ | 05 MPa | (813) |  |  | $P=0$ | MPa | (99.6) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\left.7{ }^{\prime} \mathrm{C}\right)$ | )( $\left.\mathrm{m}^{3} / \mathrm{kg}\right)$ | U(2)/8) | h(Uls) | S(L/g-K) | $7 \mathrm{C})$ | $1\left(n^{3} / 48\right)$ | U2Jk) | HWlkg) | (1)\%-K) | T'C) | $1\left(\nabla^{\prime} / \mathrm{kg}\right)$ | (20kg) | M(llyg) | S(U)/g-K) |
| 458 | 14.6701 | 20172 | 26519 | 8.148 | 81.3 | 1200 | 26812 | 26652 | 1.9080 | \%6\% | 16939 | 2056 | 26750 | 13568 |
| 50 | 149139 | 2413 | 29024 | 8.175 |  |  |  |  |  |  |  |  |  |  |
| 100 | 17,1984 | 2155 | 2685 | 8.458 | 100 | 3189 | 2115 | 3684 | 16053 | 100 | 1489 | 2062 | 26758 | 13610 |
| 150 | 19.5182 | 2097.9 | 27810 | 88.592 | 150 | 3897 | 245.7 | $27 \mathrm{Mo2}$ | 1,9113 | 150 | 1.8967 | 2929 | 27766 | 76188 |
| 300 | 21.808 | 3561.3 | 23796 | 8 Cm 97 | 30 | 4368 | 3060.0 | 28778 | 8.159 | 370 | 2.1721 | 35512 | 23753 | 751\% |
| 250 | 24.1361 | 278.1 | 3714 | 8.015 | 250 | 4.806 | 2735.1 | 29761 | 83868 | 230 | 2 Ack | 27319 | 20745 | 10546 |
| 300 | 26.46\% | 23123 | 3046 | 4387 | 300 | 53840 | 2811.6 | 30588 | 853\% | 300 | 2.638 | 28106 | 30745 | 83172 |
| 350 | 28.746 | 25060 | 3175 | 4.2513 | 340 | 5.768 | $2 \mathrm{cos.4}$ | 31768 | 8.70\% | 380 | 28710 | $2 \mathrm{Ess.7}$ | 3178.8 | 8.366 |
| 430 | 31.6631 | 2065 | 12799 | 9604 | 25 | 63014 | 28859 | 3193 | 8.5699 | 400 | 1.1087 | 29583 | 1278 | 8555 |
| 450 | 33.3714 | 30503 | 31440 | 2.75.4 | 450 | 6.6717 | 30089 | 33835 | 4.6151 | 450 | 3134 | 3005.4 | 3808 | 86945 |
| 500 | 35676 | 31929 | 3469 | 4.898 | 50 | 7.1388 | 31826 | 38093 | 9.1566 | 300 | 3.568 | 3182 | 358.7 | 88361 |
| 550 | 3798\% | 3817.2 | 3597.1 | 10.034 | 580 | 7.9057 | 3817.0 | 39068 | 9.213 | 580 | 3.708 | 38156 | 3956 | 8970 |
| 600 | 40.2985 | 3013 | $3 \times 63$ | 12.163 | 60) | 8.0576 | 303.1 | $3 \times 60$ | 9.3301 | 600 | 4.819 | 31028 | 37086 | 90088 |
| 650 | 426055 | 3312 | 3172 | 10.2166 | 650 | 85195 | 33010 | 38169 | 9.4.36 | 650 | 4.250 | 3000.7 | 31166 | 92234 |
| 700 | 4.9113 | 360.8 | 3098 | Leasbs | 700 | 8.812 | 34066 | 30097 | 9.665 | 760 | 4.200 | 360.4 | 309.4 | 9384 |
| 780 | 47.2191 | 3572.2 | 4)4.4 | 105308 | 790 | 9.4130 | 35720 | 4042 | 9.773 | 780 | 4.7309 | 35718 | 4W139 | 9.6572 |
| toto | 405309 | )0653 | 41606 | te6311 | 30) | 59047 | 36652 | 41604 | 4088 | tom | 45519 | 36650 | 41602 | 95651 |
| 850 | 51847 | 37603 | 47786 | 10.7395 | 850 | 103663 | 3700.1 | 42785 | 4.965 | 850 | 5.188 | 37000 | 2272 | 4.6759 |
| 900 | 3.1484 | 38569 | 4583 | 10449 | 900 | 108860 | 38468 | 438.2 | 10.1000 | 900 | 5.1137 | 38466 | 4380 | 2\%e0 |
| 980 | 56.4501 | 3755 | 4519.7 | 10.946 | 950 | 11.296 | 3955.1 | 4519.5 | 102014 | 950 | 58.846 | 3959.0 | 45195 | 98513 |
| 1000 | 387878 | 43552 | 4428 | 11.0428 | 100 | 11.3513 | 4059.1 | 46429 | 103000 | 1000 | 5.874 | 40550 | 4426 | 98000 |
| 1050 | 61.265 | 41868 | 47675 | 11.1399 | 1060 | 12.2129 | 4158 | 4\%76.4 | 103960 | 1050 | 6.1061 | 41866 | 47673 | 10.5761 |
| 1160 | 61372 | 4 Nab | 45907 | 11.2395 | 1100 | 12.6745 | 4399.9 | 4 W 23 | 10.4997 | 1100 | 6337 | 4898 | 49935 | 10.169 |
| 1150 | 656858 | 4) 4.7 | 50215 | 11.3239 | 1150 | 11.130 | 43846 | 5081.4 | 10.5811 | 1150 | 56800 | 4845 | 5021.3 | 10.2651 |
| 1200 | 679885 | 46709 | 5150.7 | 11.2132 | 1200 | 115971 | 4178 | 51507 | 10.6705 | 1200 | 6.7088 | 450.7 | 5150.6 | 103504 |
| 129 | 70.851 | 4578.4 | 581.4 | 115004 | 1250 | 14.0592 | 4578.4 | 58813 | 10896 | 180 | 7/06 | 45873 | 531.2 | 10438 |
| $1300,$ | 1260s | $\begin{gathered} 4624 \\ 015 \end{gathered}$ | 5413.4 | 11.5859 | $1900$ | , 4.5088 | $4613$ $(1355$ | 54113 | 10.888 | $\begin{aligned} & 1300 \\ & P=0 \end{aligned}$ | $\frac{73604}{}$ | $\begin{aligned} & 46192 \\ & (1416) \end{aligned}$ | 5413 | 10520 |
| T'C) | H( $\left.\mathrm{m}^{3} / \mathrm{ke}\right)$ | Ulalkg) | HWlkg | S(Lkg-K) | T'C) | 11 $\left.\mathrm{m}^{3} / \mathrm{kg}\right)$ | U13kg) | MUly | 921keK) | T' ${ }^{\prime}$ ) | Il ${ }^{3} \mathrm{lkg}$ | (120kg) | H1019 | SLHe-K) |
| 1203 | -2357 | 2589.1 | 276.2 | 7.1500 | 1385 | 0.6058 | 25482 | 2724 | 6.5016 | 143.6 | (ats) | 2558.1 | 2738.1 | 68565 |
| 150 | (6999 | 2577.1 | 2160.1 | 7380 | 150 | 0.6340 | 2710 | 28512 | 7.0791 | 150 | eator | 264.4 | 27928 | 6.9505 |
| 200 | 18005 | 26546 | 2870.7 | 7.5081 | 200 | 0.7164 | 25510 | 25659 | 73131 | 200 | -5343 | 20872 | 23609 | 7.1723 |
| 250 | 1.1969 | 2751.4 | 29712 | 2.7500 | 250 | 0.5964 | 27289 | 2679 | 75150 | 230 | -6952 | 27284 | 2045 | 7304 |
| 300 | 11365 | 206s | 3072.1 | 78841 | 300 | 65753 | 2 xin 0 | 30696 | 7.7017 | 300 | -6549 | 2506.1 | 3067.1 | 75677 |
| 350 | 1.4330 | 20893 | 3173.9 | 8.064 | 350 | 0.9536 | $2 \times 859$ | 31720 | 78750 | 350 | - 27145 | 2084 | 31700 | 72399 |
| 400 | 1.5498 | 2067.1 | 32770 | 8.2236 | 450 | 1.0315 | 29660 | 32755 | 880347 | 400 | 0.7725 | 29649 | 32719 | 79002 |
| 450 | 1.6685 | 30tes | 381.6 | 8.374 | 450 | 1.1092 | 30475 | 33003 | 8.18 \% | 450 | - 4311 | 30456 | 3390 | 8805 |
| 500 | 1.818 | 11114 | 38179 | 85158 | 350 | 11587 | 31315 | 34856 | 8.1271 | 50 | -x30t | 31208 | 3855 | 8.553 |
| 550 | 18973 | 32159 | 3958.4 | 8.6500 | 580 | 1.2641 | 32153 | 35945 | 8.4633 | 580 | 6.9475 | 3214.5 | 3593.6 | 8388 |
| 600 | 20130 | 33022 | 3704.8 | 8.702 | 600 | 13414 | 33016 | 37040 | 85014 | 600 | 1005\% | 33010 | 30032 | 8.850 |
| 66\% | 2.1287 | 33502 | 35159 | 88030 | 650 | 1.4186 | 3350.7 | 38153 | 䞼7159 | 650 | 1.66\% | 3360.1 | 35146 | 8850 |
| 70 | 2340 | 31099 | 3028. | 40935 | N0 | 1.4058 | 1095 | 30582 | 8534 | 500 | 1.1819 | 3\% ${ }^{\text {a }}$ | 3076 | 8.7012 |
| 750 | 23999 | 3571.4 | 4543.4 | 9138 | 750 | 1.5729 | 3571.0 | 20429 | 8.5494 | 750 | 1.1794 | 3575 | 4042.4 | 8816 |
| 800 | 2.4755 | M6447 | 41598 | 9285 | 80 | 1.6500 | 36643 | 4159.3 | 9.6604 | 800 | 12313 | 36619 | 41588 | 80273 |
| 650 | 25710 | 3799.5 | 42778 | 93559 | 850 | 17271 | 37593 | 4271.4 | 9.1659 | 850 | 12851 | 3750.0 | 4277.0 | 90.050 |
| 90 | 2706 | 30563 | 49956 | 9.55\% | 950 | 13042 | 38560 | 4993 | 9.2754 | 900 | 13530 | 3855.7 | 4366 | 9.1384 |
| \$50 | 28221 | 3084.7 | 4519.1 | 98612 | 980 | 1.812 | 3984.4 | 49188 | 9.3739 | 950 | 1.4108 | 3054.2 | 45185 | 9305 |
| 1060 | 29375 | 43548 | 4542.3 | 96599 | 100 | 19562 | 40545 | 26420 | 9.47\% | 1000 | 126\% | 40543 | 4641.7 | 9175 |
| 156 | 30570 | 41564 | 4757.0 | 97560 | 1060 | 20352 | 4158 | 45667 | 9.56st | 1050 | 15354 | 41559 | 47565 | 9.855 |
| 1150 | 3.688 | 4259.6 | 25913 | 98097 | 1100 | 21122 | 4250.4 | 25031 | 9.6631 | 150 | 15841 | 42502 | 25928 | 95895 |
| 1150 | 32839 | $5 \times 43$ | 5021.1 | 99411 | 1150 | 21802 | 4364.1 | S0809 | 9.7588 | 1150 | 1.8419 | 4889 | 5030.7 | 98309 |
| 1200 | 33994 | 45785 | 5150.4 | thenst | 1290 | 2 $\times 662$ | 41583 | 51502 | 9.8431 | 1200 | 1.0997 | 4072.1 | 51500 | 971t |
| 1250 | 35148 | $457 \times 1$ | 531.1 | 10.1176 | 1250 | 2342 | 4577.9 | $53 \times 19$ | 9.9303 | 1230 | 1.7574 | 45778 | 5350.7 | 97075 |
| 1360 | 3.6302 | 48575 | 5413.1 | 10.20189 | 1360 | 20002 | 4656.9 | 54129 | 10.0156 | 1300 | 18152 | 486.7 | 54128 | 98888 |


| $P=9.00 \mathrm{MPa}$ |  | (303.4) |  |  | $P=10.00 \mathrm{MPa}$ |  | (311.0) |  |  | $P=12.50 \mathrm{MPa}$ |  | (327.8) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $7\left({ }^{\circ} \mathrm{C}\right)$ | $V\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ | $U(\mathrm{~kJ} / \mathrm{kg})$ | $H(\mathrm{k} / \mathrm{kg})$ | $S(\mathrm{~kJ} / \mathrm{kg}-\mathrm{K})$ | $7\left({ }^{\circ} \mathrm{C}\right)$ | $V\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ | $U(\mathrm{~kJ} / \mathrm{kg})$ | $H(\mathrm{~kJ} / \mathrm{kg})$ | $S(\mathrm{~kJ} / \mathrm{kg}-\mathrm{K})$ | $T\left({ }^{\circ} \mathrm{C}\right)$ | $1\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ | $U(\mathrm{k} / \mathrm{kg})$ | $H(\mathrm{k} / \mathrm{kg})$ | $S(\mathrm{~kJ} / \mathrm{kg}-\mathrm{K})$ |
| 303.4 | 0.0205 | 2558.5 | 2742.9 | 5.6791 | 311.0 | 0.0180 | 2545.2 | 2725.5 | 5.6160 | 327.8 | 0.0135 | 2505.61 | 2674.31 | 5.4638 |
| 350 | 0.0258 | 2724.9 | 2957.3 | 6.0380 | 350 | 0.0224 | 2699.6 | 2924.0 | 5.9459 | 350 | 0.0161 | 2624.8 | 2826.6 | 5.7130 |
| 400 | 0.0300 | 2849.2 | 3118.8 | 6.2876 | 400 | 0.0264 | 2833.1 | 3097.4 | 6.2141 | 400 | 0.0200 | 2789.6 | 3040.0 | 6.0433 |
| 450 | 0.0335 | 2956.3 | 3258.0 | 6.4872 | 450 | 0.0298 | 2944.5 | 3242.3 | 6.4219 | 450 | 0.0230 | 2913.7 | 3201.4 | 6.2749 |
| 500 | 0.0368 | 3056.3 | 3387.4 | 6.6603 | 500 | 0.0328 | 3047.0 | 3375.1 | 6.5995 | 500 | 0.0256 | 3023.2 | 3343.6 | 6.4650 |
| 550 | 0.0399 | 3153.0 | 3512.0 | 6.8164 | 550 | 0.0357 | 3145.4 | 3502.0 | 6.7585 | 550 | 0.0280 | 3126.1 | 34765 | 6.6317 |
| 600 | 0.0429 | 3248.4 | 3634.1 | 6.9605 | 600 | 0.0384 | 3242.0 | 3625.8 | 6.9045 | 600 | 0.0303 | 3225.8 | 3604.6 | 6.7828 |
| 650 | 0.0458 | 3343.4 | 3755.2 | 7.0953 | 650 | 0.0410 | 33379 | 3748.1 | 7.0408 | 650 | 0.0325 | 3324.1 | 3730.2 | 6.9227 |
| 700 | 0.0486 | 3438.8 | 3876.1 | 7.2229 | 700 | 0.0436 | 3434.0 | 3870.0 | 7.1693 | 700 | 0.0346 | 3422.0 | 3854.6 | 7.0539 |
| 750 | 0.0514 | 3534.9 | 3997.3 | 7.3443 | 750 | 0.0461 | 3530.7 | 3992.0 | 7.2916 | 750 | 0.0367 | 3520.1 | 3978.6 | 7.1782 |
| 800 | 0.0541 | 3632.0 | 4119.1 | 7.4606 | 800 | 0.0486 | 3628.2 | 4114.5 | 7.4085 | 800 | 0.0387 | 3618.7 | 41028 | 7.2967 |
| 850 | 0.0569 | 3730.2 | 4241.9 | 7.5724 | 850 | 0.0511 | 3726.8 | 4237.8 | 7.5207 | 850 | 0.0407 | 3718.3 | 4227.5 | 7.4102 |
| 900 | 0.05\% | 3829.6 | 4365.7 | 7.6802 | 900 | 0.0535 | 3826.5 | 4362.0 | 7.6290 | 900 | 0.0427 | 3818.9 | 4352.9 | 7.5194 |
| 950 | 0.0622 | 3930.3 | 4490.6 | 7.7844 | 950 | 0.0560 | 3927.5 | 4487.3 | 7.7335 | 950 | 0.0447 | 3920.6 | 4479.2 | 7.6249 |
| 1000 | 0.0649 | 4032.4 | 4616.7 | 7.8855 | 1000 | 0.0584 | 4029.9 | 4613.8 | 7.8349 | 1000 | 0.0466 | 4023.5 | 4606.5 | 7.7269 |
| 1050 | 0.0676 | 4135.9 | 4744.0 | 7.9836 | 1050 | 0.0608 | 4133.5 | 4741.4 | 7.9332 | 1050 | 0.0486 | 4127.7 | 47349 | 7.8258 |
| 1100 | 0.0702 | 4240.6 | 4872.7 | 8.0790 | 1100 | 0.0632 | 4238.5 | 4870.3 | 8.0288 | 1100 | 0.0505 | 4233.1 | 4864.5 | 7.9219 |
| 1150 | 0.0729 | 4346.8 | 5002.5 | 8.1719 | 1150 | 0.0656 | 4344.8 | 5000.4 | 8.1219 | 1150 | 0.0524 | 4339.8 | 4995.1 | 8.0154 |
| 1200 | 0.0755 | 4454.2 | 5133.6 | 8.2625 | 1200 | 0.0679 | 4452.3 | 5131.7 | 8.2126 | 1200 | 0.0543 | 4447.7 | 5127.0 | 8.1065 |
| 1250 | 0.0781 | 4562.9 | 52660 | 8.3508 | 1250 | 0.0703 | 4561.2 | 5264.2 | 8.3010 | 1250 | 0.0562 | 4556.9 | 5260.0 | 8.1952 |
| $\begin{aligned} & 1300 \\ & P=1 . \end{aligned}$ | 0.08007 00 MPa | $\begin{gathered} 46729 \\ (342.2) \end{gathered}$ | 5399.5 | 8.4370 | $\begin{aligned} & 1300 \\ & P=1 \end{aligned}$ | $\stackrel{0.0727}{7.50 \mathrm{MPa}}$ | 4671.3 <br> (354.7) | 5397.9 | 8.3874 | $\begin{aligned} & 1300 \\ & P=2 \end{aligned}$ | $\begin{aligned} & 00581 \\ & 00 \mathrm{MPa} \end{aligned}$ | 4667.3 <br> (365.8) | 5394.1 | 8.2819 |
| $\left.T{ }^{\circ} \mathrm{C}\right)$ | $V\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ | $U(\mathrm{~kJ} / \mathrm{kg})$ | $H(\mathrm{k} / \mathrm{kg})$ | $5(\mathrm{~kJ} / \mathrm{kg}-\mathrm{K})$ | $\left.7{ }^{\circ} \mathrm{C}\right)$ | $V\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ | $U(\mathrm{~kJ} / \mathrm{kg})$ | $H(\mathrm{k} / \mathrm{kg})$ | $S(\mathrm{~kJ} / \mathrm{kg}-\mathrm{K})$ | $\left.T{ }^{\circ} \mathrm{C}\right)$ | $V\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ | $U(\mathrm{k} / \mathrm{kg})$ | $H(\mathrm{~kJ} / \mathrm{kg})$ | S(kJ/kg-K) |
| 342.2 | 0.0103 | 2455.6 | 2610.7 | 5.3106 | 354.7 | 0.0079 | 2390.5 | 2529.3 | 5.1431 | 365.8 | 0.0059 | 2295.0 | 2412.4 | 4.9315 |
| 350 | 0.0115 | 2520.9 | 2693.1 | 5.4437 |  |  |  |  |  |  |  |  |  |  |
| 400 | 0.0157 | 2740.6 | 2975.7 | 5.8819 | 400 | 0.0125 | 2684.3 | 2902.4 | 5.7211 | 400 | 0.0100 | 26179 | 2816.9 | 55525 |
| 450 | 0.0185 | 2880.7 | 3157.9 | 6.1434 | 450 | 0.0152 | 2845.4 | 3111.4 | 6.0212 | 450 | 0.0127 | 28072 | 3061.7 | 5.9043 |
| 500 | 0.0208 | 2998.4 | 3310.8 | 6.3480 | 500 | 0.0174 | 2972.4 | 3276.7 | 6.2424 | 500 | 0.0148 | 2945.3 | 3241.2 | 6.1446 |
| 550 | 0.0229 | 3106.2 | 3450.4 | 6.5230 | 550 | 0.0193 | 3085.8 | 3423.6 | 6.4266 | 550 | 0.0166 | 3064.7 | 33\%.1 | 63389 |
| 600 | 0.0249 | 3209.3 | 3583.1 | 6.67\% | 600 | 0.0211 | 3192.5 | 3561.3 | 6.5890 | 600 | 0.0182 | 3175.3 | 3539.0 | 6.5075 |
| 650 | 0.0268 | 3310.1 | 3712.1 | 6.8233 | 650 | 0.0227 | 3295.8 | 3693.8 | 6.7366 | 650 | 0.0197 | 3281.4 | 3675.3 | 6.6593 |
| 700 | 0.0286 | 3409.8 | 3839.1 | 6.9572 | 700 | 0.0243 | 3397.5 | 3823.5 | 6.8734 | 700 | 0.0211 | 3385.1 | 3807.8 | 6.7990 |
| 750 | 0.0304 | 3509.4 | 3965.2 | 7.0836 | 750 | 0.0259 | 3498.6 | 3951.7 | 7.0019 | 750 | 0.0225 | 3487.7 | 3938.1 | 69297 |
| 800 | 0.0321 | 3609.2 | 4091.1 | 7.2037 | 800 | 0.0274 | 3599.7 | 4079.3 | 7.1236 | 800 | 0.0239 | 3590.1 | 4067.5 | 7.0531 |
| 850 | 0.0338 | 3709.8 | 4217.1 | 7.3185 | 850 | 0.0289 | 3701.2 | 42068 | 7.2398 | 850 | 0.0252 | 3692.6 | 4196.4 | 7.1705 |
| 900 | 0.0355 | 3811.2 | 4343.7 | 7.4288 | 900 | 0.0303 | 3803.4 | 4334.5 | 7.3511 | 900 | 0.0265 | 3795.7 | 4325.4 | 72829 |
| 950 | 0.0372 | 3913.6 | 4471.0 | 7.5350 | 950 | 0.0318 | 3906.6 | 4462.9 | 7.4582 | 950 | 0.0278 | 3899.5 | 4454.7 | 73909 |
| 1000 | 0.0388 | 4017.1 | 4599.2 | 7.6378 | 1000 | 0.0332 | 4010.7 | 4592.0 | 7.5616 | 1000 | 0.0290 | 4004.3 | 4584.7 | 7.4950 |
| 1050 | 0.0404 | 4121.8 | 4728.4 | 7.7373 | 1050 | 0.0346 | 4115.9 | 4721.9 | 7.6617 | 1050 | 0.0303 | 4110.0 | 4715.4 | 7.5957 |
| 1100 | 0.0421 | 4227.7 | 4858.6 | 7.8339 | 1100 | 0.0360 | 4222.3 | 4852.8 | 7.7588 | 1100 | 0.0315 | 4216.9 | 4846.9 | 7.6933 |
| 1150 | 0.0437 | 4334.8 | 4989.9 | 7.9278 | 1150 | 0.0374 | 4329.8 | 4984.6 | 78531 | 1150 | 0.0327 | 4324.8 | 4979.4 | 7.7880 |
| 1200 | 0.0453 | 4443.1 | 5122.3 | 8.0192 | 1200 | 0.0388 | 4438.4 | 5117.5 | 7.949 | 1200 | 0.0340 | 44338 | 51128 | 78802 |
| 1250 | 0.0469 | 4552.6 | 5255.7 | 8.1083 | 1250 | 0.0402 | 45483 | 5251.5 | 8.0343 | 1250 | 0.0352 | 4544.0 | 5247.2 | 7.9699 |
| 1309 | 00485 | 4663.2 | 5390.3 | 8.1952 | 1300 | 0.0416 | 4659.2 | 53864 | 8.1215 | 1300 | 000364 | 46552 | 5382.6 | 80574 |

## Properties of Selected Compounds

Heat capacities are values for ideal gas at 298 K and should be used for order of magnitude calculations only. See appendices for temperature-dependent formulas and constants.

| ID | Compound | $\begin{gathered} T_{c} \\ (\mathrm{~K}) \end{gathered}$ | $\begin{gathered} P_{c} \\ (\mathrm{MPa}) \end{gathered}$ | $\omega$ | $\underset{\mathrm{g} / \mathrm{cm}^{3}}{\rho}$ | MW | $C_{P}{ }^{i g / R}$ | $\underset{\left(\mathrm{J} / \mathrm{cm}^{3}\right)^{5}}{\delta}$ | $\begin{gathered} \alpha \\ \left(\mathrm{J} / \mathrm{cm}^{3}\right)^{5} \end{gathered}$ | $\begin{gathered} \beta \\ \left(\mathrm{J} / \mathrm{cm}^{3}\right)^{n} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 902 | HYDROGEN | 33.3 | 1.297 | -0.215 | 0.20 | 2 | 3.507 | 2.0 | 0 | 0 |
| 905 | Nitrogen | 126.1 | 3.394 | 0.040 | 0.88 | 28 | 3.500 | 5.3 | 0 | 0 |
| 908 | CARBON MONOXIDE | 132.9 | 3.499 | 0.066 | 0.88 | 28 | 3.505 | 6.3 | 0 | 0 |
| 909 | CARBON DIOXIDE | 304.2 | 7.382 | 0.228 | 1.18 | 44 | 4.456 | 14.6 | 1.87 | 0 |
| Nasty gases |  |  |  |  |  |  |  |  |  |  |
| 1922 | HYDROGEN SULFIDE | 373.5 | 8.937 | 0.081 | 0.95 | 34 | 4.115 | 18.0 | 3.19 | 3.19 |
| 1938 | CARBON DISULFIDE | 552 | 7.800 | 0.115 | 1.26 | 76 | 4.109 | 20.4 | 0.59 | 0.33 |
| 1904 | HYDROGEN CHLORIDE | 324.6 | 8.200 | 0.120 | 1.19 | 36.5 | 3.551 | 22.0 | $22.0{ }^{\circ}$ | 0 |
| 1771 | HYDROGEN CYANIDE | 456.8 | 5.320 | 0.407 | 0.68 | 27 | 4.330 | 24.8 | 3.00 | 3.00 |
| Miscellaneous compounds |  |  |  |  |  |  |  |  |  |  |
| 1051 | ACETONE | 508.2 | 4.701 | 0.306 | 0.79 | 58 | 8.96 | 19.6 | 0.00 | 11.14 |
| 1772 | ACETONITRILE | 545.5 | 4.833 | 0.353 | 0.78 | 44 | 6.28 | 24.1 | 3.49 | 8.98 |
| 1252 | ACETIC ACID | 592.7 | 5.786 | 0.462 | 1.04 | 60 | 15.01 | 19.0 | 24.03 | 7.50 |
| 1911 | AMMONIA | 406.6 | 11.270 | 0.252 | 0.68 | 17 | 4.29 | 29.2 | 2.11 | 8.44 |
| 1921 | WATER | 647.3 | 22.120 | 0.344 | 1.00 | 18 | 4.04 | 47.9 | 50.13 | 15.06 |

# ANSWERS Quiz 4 <br> Chemical Engineering Thermodynamics <br> February 11, 2016 

(P4.2) Initial (each $x$ represents 5 molecule)

| xxxx |  |
| :--- | :--- |
|  |  |

Final

| $\mathbf{x}$ | $\mathbf{x}$ |
| :--- | :--- |
| $\mathbf{x}$ | $\mathbf{x}$ |

Create a space with a three empty boxes for the initial state. The number of molecules is too small to use Stirling's approximation.
$\mathrm{p} 1=20!/(20!0!0!0!)=1$
p2 $=20!/(5!5!5!5!)=20^{*} 19^{*} 18^{*} 17^{*} 16^{*} 15^{*} 14^{*} 13 * 12 * 11^{*} 10^{*} 9 * 8 * 7 * 6 /\left(5 * 4^{*} 3 * 2\right)^{\wedge} 3=$
11732745024
$\Delta \mathrm{S} / \mathrm{k}=\ln (\mathrm{p} 2 / \mathrm{p} 1)=\ln (11732745024)=23.18$
This can also be calculated from the volume ratio,
$\Delta \mathrm{S} / \mathrm{k}=20 \ln \left(\mathrm{~V}_{2} / \mathrm{V}_{1}\right)=20(1.39)=27.7$
The increase of 4.53 k in $\Delta \mathrm{S}$ is due to release of the constraint of confinement of the groups of five atoms in the four boxes.
(4.09) Airplanes are launched from aircraft carriers by means of a steam catapult.

Solution : It cannot generate more than the adiabatic reversible result. But in principle it could generate at most the adiabatic reversible result.

Energy Balance : $\mathrm{d}(\mathrm{mU})=\mathrm{Q}+\mathrm{W}=\mathrm{W}$
Entropy balance : $\Delta \mathrm{S}=0$
State 1: $\mathrm{U}_{1}=2880.7$
State 2 : Sat liq $U-604.22 \mathrm{~S}=1.7765$
$\mathrm{S}_{1}=6.1434$
Sat Vap $U=2553.1 \mathrm{~S}=6.8955$
$V_{1}=18.5 \mathrm{~cm}^{3} / \mathrm{g}$
$\mathrm{V}^{\text {sal }}=1.08 \mathrm{~cm}^{3} / \mathrm{g}, \mathrm{V}^{\text {aiV }}=462 \mathrm{~cm}^{3} / \mathrm{g}$

Therefore, work done by gas
$\mathrm{q}=(6.1434-1.7765) /(6.8955-1.7765)=0.853$
$\mathrm{U}_{2}=0.853 * 2553.1+0.147 * 604.2=2266.6$
$W_{\text {pas }}=2266.6-2880.7=-614.1 \mathrm{~kJ} / \mathrm{kg}$
$\underline{W}_{\text {gas }}=270 *(-614.1)=-165,800 \mathrm{~kJ}$
Some of the work is done on the atmosphere, need $\mathrm{P}_{\text {atm }} \Delta \underline{\mathrm{V}}$
$\mathrm{V}^{\mathrm{r}}=1.085+0.853(461)=394 \mathrm{~cm}^{3} / \mathrm{g}$
$\underline{W}_{\mathrm{EC}, \mathrm{atm}}=-\mathrm{P}_{\mathrm{atm}}\left(\underline{\mathrm{V}}^{\mathrm{r}}-\underline{\mathrm{V}}^{\mathrm{i}}\right)=-0.1 \mathrm{MPa}^{*}(270 \mathrm{E} 3 \mathrm{~g})(394-185)=10,139 \mathrm{~kJ}$
Net work (ignoring acceleration of piston -- mass not given) $=-165,800+10,139$
$=-156,000 \mathrm{~J}$
For the Airplane, calculate the KE necessary at $350 \mathrm{~km} / \mathrm{h}$
$\mathrm{W}_{\mathrm{S}}=\int \mathrm{d}\left(\mathrm{m}\left(\mathrm{v}^{2} / 2\right)\right)$
$=\mathrm{m}\left(\mathrm{v}^{\mathrm{f}}\right)^{2} / 2=30000 \mathrm{~kg}^{*}(350000 \mathrm{~m}-\mathrm{hr} / 3600 \mathrm{hr}-\mathrm{s})^{2} / 2$
$=141,782 \mathrm{~kJ}$
$156,000>142,000$ Therefore the catapult can generate enough work to launch the plane.
Or, one could calculate the final plane velocity for $156,000 \mathrm{~kJ}$.
$\operatorname{Sqrt}\left((1.56 \mathrm{E} 8 \mathrm{~J})^{*} 2 / 30 \mathrm{E} 3 \mathrm{~kg}\right)=102 \mathrm{~m} / \mathrm{s}=367 \mathrm{~km} / \mathrm{hr}$, plenty of speed.

